



A. Additional codes

The code to create the mesh in Chapter 5:

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1 function foilgmsh(archi , alfa , yplus , eter , Re,M,T0,N,bump)
2 %foilgmsh( archi , alfa , yplus , eter ,Re,M,T0,N,bump)
3 %
4 %foilgmsh will create a GEO file with all necessary instructions to mesh an
5 % airfoil geometry only with hexahedra in Gmsh, departing from a set of points
6 % defining the airfoil section contour. So far this code can only deal with
7 % monoelement airfoils and 2D simulations for finite volume CFD codes.
8 %The on-screen output displays a summary of the input, some statistics of the mesh
9 % to be created and useful information for definition of the case in CFD
10 % softwares , specially Code_Saturne .
11 %
12 %- archi: string which defines the complete name of the airfoil coordinates file.
13 % The coordinates must be given in Xfoil format starting from the trailing edge
14 % and circling counterclockwise. The coordinates don't need to be
15 % adimensionalized , but the program won't do it either , as the airfoil chord
16 % will be estimated automatically from it . The author consider's this is useful
17 % to compare further results with experimental data. The coordinates can be
18 % off-centered by small amounts.
19 %
20 %- alfa: desired angle of attack in degrees. The mesh generated will be so in wind
21 % axis system , where wind velocity coincides in sense and direction with the
22 % positive X axis , so when defining inlet speed, Y and Z components should be
23 % zero. Also , the section plane coincides with the mesh XY plane.
24 %
25 %- yplus: desired y+ value around the airfoil. Spacing between susecuent cells
26 % normal to the airfoil surface is done with an authomatically defined geometric
27 % progression .
28 %
29 %- eter: string defining material medium where airfoil is submerged. Only three
30 % possibilities are allowed , 'a' for normal air , 'h' for distilled water and 'n'
31 % for nitrogen .
32 %
33 %- Re: Reynolds number based on airfoil chord and freestream speed. The reference
34 % chord and that of the airfoil in the coordinates file must coincide.
35 %
36 %- M: if the medium is air or nitrogen , it is the Mach number. If the medium is
37 % water , it is the freestream speed magnitude in m/s. Although the applied
38 % formulas hold for transonic and supersonic flows , the resulting mesh might not
39 % be suitable for those cases. Compressible fully subsonic flows should not be a
40 % problem .
41 %

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20 %-- T0: if the medium is air or nitrogen, it is the stagnation temperature in
   Kelvin degrees. If the medium is water, it is the non-stagnated flow
   temperature in Celsius degrees.
21 %
22 %- N: four integers vector whre N(1) is the number of hexahedra along the airfoil
   chord, therefore the whole contour of the airfoil will be discretized in
   2*N(1) elements. N(2) is the number of elements normal to the chord and inside
   a semiellipse closely enclosing the airfoil (a value between 25 and 100 should
   suffice for most applications). N(3) is the number of elements into which the
   horizontal leading edge-inlet and trailing edge-outlet gaps will be
   discretized. N(4) is similar to N(3) but applied to the vertical gaps between
   the airfoil and the top/bottom walls defining the box.
23 %
24 %- bump: a value which defines the mesh concentration degree around the leading
   and trailing edge. If bump=1 the cell lenghts will be uniform along the
   airfoil contour, if bump>1 the elements will be concentrated around the
   midchord. If 0<bump<1 the elements will concentrate around the edges, and
   don't be surprised if you need very low values like 0.1 or less to achieve a
   noticeable concentration.
25 %
26 %-To mesh, simply open in Gmsh the generated GEO file , go to Mesh with the menu or
   by pressing 'm' and click on "3D". Save the mesh as a MED file for use with
   Code_Saturne (remember to apply 'check cell orientation' in the GUI or
   preprocessor). The generated groups are "inlet", "outlet", "airfoil",
   "symmetry" and "walls".
27 %-The on-screen output text provides information to define all necessary variables
   in CS's GUI. The hydraulic diameter value is just a dummy number suitable to
   initialize properly the turbulence model for external flows.
28 %
29 %-Send some feedback if you wish to cesar-vecchio@gmx.com (I also accept Ferraris
   and Porsches). I hope you find this software useful.
30 %-----
31 %-Cesar A. Vecchio Toloy
32 %-----
33 %-Disclaimer: I am giving you this software as is fully for free. I will not be
   responsible for any harm of any kind this code and the uses you give to it may
   cause. You are using this code under your own responsability and risk.
34
35 more off
36
37 N = N+1; %number of nodes on upper and lower surface
38 alfa = -alfa*pi/180; %conversion to radians and Gmsh references
39 inic = load(archi); %loading coordinates file...
40 [m void] = size(inic);
41 inic(1,2)=(inic(1,2)+inic(m,2))/2; %the trailing edge is closed. Sorry for the
   inconvenience.
42 percor=inic(1:m-1,:); %the (now) extra trailing edge point is removed.
43 m=m-1;disp(m)
44 z0 = 0;
45 [maxx posmaxx] = max(percor(:,1));
46 [minx posminx] = min(percor(:,1));
47 cuerda = maxx-minx; %computation of airfoil chord
48 [maxy posmaxy] = max(percor(:,2));
49 [miny posminy] = min(percor(:,2));
50
51 fid = fopen(strcat(archi,'.geo'), 'w'); %opening the output file
52

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53 %writing the points which define the airfoil
54 for i = 1:m
55 fprintf(fid , 'Point(%i) =
56     {%.10g,%.10g,%.10g,%.10g};\n',i , percor(i,1) , percor(i,2) , z0 , cuerda/100);
57 end
58
59 %writing the points which define the enclosing semiellipse
60 fprintf (fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n',
61     m+1,minx-cuerda/20,0,z0,cuerda/25);
62 fprintf (fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n',
63     m+2,maxx,maxy+cuerda/4,z0,cuerda/25);
64 fprintf (fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n',
65     m+3,maxx,miny-cuerda/4,z0,cuerda/25);
66
67 fprintf (fid , 'Spline(1) = {'); %defining an interpolating spline for the upper
68     surface
69 for i = posminx:m
70 fprintf (fid , '%i , ', i);
71 end
72 %The following and all the lines where you see 'Transfinite' is a way of
73 %indicating to Gmsh that a structured mesh will be made.
74 fprintf (fid , '%i}; Transfinite Line{1} = %i Using Bump %f;\n', 1,N(1),bump);
75 fprintf (fid , 'Spline(2) = {'); %lower surface interpolating spline
76 for i = 1:posminx-1
77 fprintf (fid , '%i , ', i);
78 end
79 fprintf (fid , '%i}; Transfinite Line{2} = %i Using Bump %f;\n', posminx,N(1),bump);
80
81 %Defining the lines of our enclosing semiellipse
82 fprintf (fid , 'Ellipse(3) = {%i,%i,%i,%i}; Transfinite Line{3} = %i Using
83     Progression 1;\n', m+1,1,posminx,m+2,N(1));
84 fprintf (fid , 'Ellipse(4) = {%i,%i,%i,%i}; Transfinite Line{4} = %i Using
85     Progression 1;\n', m+1,1,posminx,m+3,N(1));
86 %Calculating minimum cell distance from wall and geometric progression with
87 %subfunctions
88 Ymin = ypar (yplus , cuerda , Re , M , T0 , eter); Prog5 =
89     mindist(Ymin,norm(percor(posmaxx,:)-[maxx,maxy+cuerda/4]),N(2));
90 fprintf (fid , 'Line(5) = {%i,%i}; Transfinite Line{5} = %i Using Progression
91     %.10g;\n', 1,m+2,N(2),Prog5);
92 Prog6 = mindist(Ymin,norm(percor(posmaxx,:)-[maxx,miny-cuerda/4]),N(2));
93 fprintf (fid , 'Line(6) = {%i,%i}; Transfinite Line{6} = %i Using Progression
94     %.10g;\n', 1,m+3,N(2),Prog6);
95 Prog7 = mindist(Ymin,norm(percor(posminx,:)-[minx-cuerda/20,0]),N(2));
96 fprintf (fid , 'Line(7) = {%i,%i}; Transfinite Line{7} = %i Using Progression
97     %.10g;\n', posminx,m+1,N(2),Prog7);
98
99 %2D surfaces are created from the available liens so far
100 fprintf (fid , 'Line Loop(1) = {-2,5,-3,-7};\n');
101 fprintf (fid , 'Ruled Surface(1) = {1};\n');
102 fprintf (fid , 'Transfinite Surface(1) = {%i,%i,%i,%i};\n', 1,posminx,m+1,m+2);
103 fprintf (fid , 'Line Loop(2) = {1,6,-4,-7};\n');
104 fprintf (fid , 'Ruled Surface(2) = {2};\n');
105 fprintf (fid , 'Transfinite Surface(2) = {%i,%i,%i,%i};\n', 1,posminx,m+1,m+3);
106
107 %Let's tell Gmsh to rotate the airfoil+semielipse our desired angle of attack
108 fprintf (fid , 'Rotate {{0,0,1},{%.10g,0,0},%.10g} {Surface{1,2};}\n',
109     minx+cuerda/2,alfa);

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96
97 %Now some points to define the flowfield boundaries. Notice the resulting box will
98 % be 15*cuerda long and 8*cuerda high.
99 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
100      m+4,maxx-(1-cos( alfa ))*cuerda/2-sin( alfa )*(cuerda/4+maxy) ,4*cuerda ,z0 ,cuerda );
101 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
102      m+5,minx-2*cuerda ,4*cuerda ,z0 ,cuerda );
103 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
104      m+6,minx-4*cuerda ,4*cuerda ,z0 ,cuerda );
105 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
106      m+7,minx-4*cuerda ,0-0.55*cuerda*sin( alfa ) ,z0 ,cuerda );
107 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
108      m+8,minx-4*cuerda ,-4*cuerda ,z0 ,cuerda );
109 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
110      m+9,minx-2*cuerda ,-4*cuerda ,z0 ,cuerda );
111 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
112      m+10,maxx-(1-cos( alfa ))*cuerda/2-sin( alfa )*(-cuerda/4+miny) ,-4*cuerda ,z0 ,cuerda );
113 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
114      m+11,maxx+10*cuerda ,-4*cuerda ,z0 ,cuerda );
115 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
116      m+12,maxx+10*cuerda ,percor( posmaxx ,2)+cos( alfa )*(miny-cuerda/4)+cuerda/2*sin( alfa ) ,z0 ,cuerda );
117 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
118      m+13,maxx+10*cuerda ,sin( alfa )*cuerda/2,z0 ,cuerda );
119 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
120      m+14,maxx+10*cuerda ,percor( posmaxx ,2)+cos( alfa )*(maxy+cuerda/4)+cuerda/2*sin( alfa ) ,z0 ,cuerda );
121 fprintf ( fid , 'Point(%i) = {%.10g,%.10g,%.10g,%.10g};\n' ,
122      m+15,maxx+10*cuerda ,4*cuerda ,z0 ,cuerda );

123 %Now we join the previous points with some lines
124 Prog =
125     mindist(Ymin*Prog7^(N(2)-1),abs(3.95*cuerda+(1-cos( alfa ))*0.55*cuerda ),N(3));
126 fprintf ( fid , 'Line(8) = {%i,%i}; Transfinite Line{8} = %i Using Progression
127     %.10g;\n' , m+1,m+7,N(3) ,Prog );
128
129 Prog = mindist(cuerda/N(1),abs(10*cuerda+(1+cos( alfa ))*0.5*cuerda ),N(3));
130 fprintf ( fid , 'Line(9) = {%i,%i}; Transfinite Line{9} = %i Using Progression
131     %.10g;\n' , 1,m+13,N(3) ,Prog );
132
133 L = 4*cuerda -(percor( posmaxx ,2)+cuerda /4)*cos( alfa )-cuerda /2*sin( alfa );
134 Prog = mindist(Ymin*Prog5^(N(2)-1),L,N(4));
135 fprintf ( fid , 'Line(10) = {%i,%i}; Transfinite Line{10} = %i Using Progression
136     %.10g;\n' , m+2,m+4,N(4) ,Prog );
137
138 L =
139     norm([minx-cuerda*2,cuerda*4]-[(minx-cuerda/20)-(1-cos( alfa ))*0.55*cuerda ,percor( posminx ,2)-sin( alfa )*cuerda ]);
140 Prog = mindist(Ymin*Prog7^(N(2)-1),L,N(4));
141 fprintf ( fid , 'Line(11) = {%i,%i}; Transfinite Line{11} = %i Using Progression
142     %.10g;\n' , m+1,m+5,N(4) ,Prog );
143
144 L =
145     norm([minx-cuerda*2,cuerda*4]-[(minx-cuerda/20)-(1-cos( alfa ))*0.55*cuerda ,percor( posminx ,2)-sin( alfa )*cuerda ]);
146 Prog = mindist(Ymin*Prog6^(N(2)-1),L,N(4));
147 fprintf ( fid , 'Line(12) = {%i,%i}; Transfinite Line{12} = %i Using Progression
148     %.10g;\n' , m+3,m+10,N(4) ,Prog );
149
150 L =
151     norm([minx-cuerda*2,-cuerda*4]-[(minx-cuerda/20)-(1-cos( alfa ))*0.55*cuerda ,percor( posminx ,2)-sin( alfa )*cuerda ]);
152 Prog = mindist(Ymin*Prog7^(N(2)-1),L,N(4));

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132 fprintf ( fid , 'Line(13) = {%,%}; Transfinite Line{13} = %i Using Progression  
133      %.10g;\n' , m+1,m+9,N(4) ,Prog );  
134  
134 Prog =  
135      mindist(cuerda/N(1),abs(10*cuerda+(1-cos( alfa ))*0.5*cuerda+sin( alfa )*(maxy+cuerda/4)),N(3));  
135 fprintf ( fid , 'Line(14) = {%,%}; Transfinite Line{14} = %i Using Progression  
136      %.10g;\n' , m+2,m+14,N(3) ,Prog );  
136  
137 Prog =  
138      mindist(cuerda/N(1),abs(10*cuerda+(1-cos( alfa ))*0.5*cuerda+sin( alfa )*(miny-cuerda/4)),N(3));  
138 fprintf ( fid , 'Line(15) = {%,%}; Transfinite Line{15} = %i Using Progression  
139      %.10g;\n' , m+3,m+12,N(3) ,Prog );  
139  
140 fprintf ( fid , 'Line(16) = {%,%}; Transfinite Line{16} = %i Using Progression  
141      1.00;\n' , m+4,m+5,N(1) );  
141  
142 fprintf ( fid , 'Line(17) = {%,%}; Transfinite Line{17} = %i Using Progression  
143      1.00;\n' , m+10,m+9,N(1) );  
143  
144 Prog =  
145      mindist((3*cuerda-cuerda/2*cos( alfa )-sin( alfa )*(maxy+cuerda/4))/N(1),2*cuerda ,N(3));  
145 fprintf ( fid , 'Line(18) = {%,%}; Transfinite Line{18} = %i Using Progression  
146      %.10g;\n' , m+5,m+6,N(3) ,Prog );  
146  
147 Prog =  
148      mindist((3*cuerda-cuerda/2*cos( alfa )-sin( alfa )*(miny-cuerda/4))/N(1),2*cuerda ,N(3));  
148 fprintf ( fid , 'Line(19) = {%,%}; Transfinite Line{19} = %i Using Progression  
149      %.10g;\n' , m+9,m+8,N(3) ,Prog );  
149  
150 Prog = mindist(cuerda/N(1),4*cuerda+cuerda*0.55*sin( alfa ),N(4));  
151 fprintf ( fid , 'Line(20) = {%,%}; Transfinite Line{20} = %i Using Progression  
152      %.10g;\n' , m+7,m+6,N(4) ,Prog );  
152  
153 Prog = mindist(cuerda/N(1),4*cuerda-cuerda*0.55*sin( alfa ),N(4));  
154 fprintf ( fid , 'Line(21) = {%,%}; Transfinite Line{21} = %i Using Progression  
155      %.10g;\n' , m+7,m+8,N(4) ,Prog );  
155  
156 Prog =  
157      mindist((3*cuerda-cuerda/2*cos( alfa )-sin( alfa )*(maxy+cuerda/4))/N(1),abs(10*cuerda+(1-cos( alfa ))*  
157 fprintf ( fid , 'Line(22) = {%,%}; Transfinite Line{22} = %i Using Progression  
158      %.10g;\n' , m+4,m+15,N(3) ,Prog );  
158  
159 Prog =  
160      mindist((3*cuerda-cuerda/2*cos( alfa )-sin( alfa )*(miny-cuerda/4))/N(1),abs(10*cuerda+(1-cos( alfa ))*  
160 fprintf ( fid , 'Line(23) = {%,%}; Transfinite Line{23} = %i Using Progression  
161      %.10g;\n' , m+10,m+11,N(3) ,Prog );  
161  
162 L = 4*cuerda+(miny-cuerda/4)*cos( alfa )+cuerda/2*sin( alfa );  
163 Prog = mindist(Ymin*Prog6^(N(2)-1),L,N(4));  
164 fprintf ( fid , 'Line(24) = {%,%}; Transfinite Line{24} = %i Using Progression  
165      %.10g;\n' , m+12,m+11,N(4) ,Prog );  
165  
166 Prog = mindist(Ymin,abs(miny-cuerda/4)*cos( alfa ),N(2));  
167 fprintf ( fid , 'Line(25) = {%,%}; Transfinite Line{25} = %i Using Progression  
168      %.10g;\n' , m+13,m+12,N(2) ,Prog );  
168  
169 Prog = mindist(Ymin,abs(maxy+cuerda/4)*cos( alfa ),N(2));
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170   fprintf (fid , 'Line(26) = {%,%i}; Transfinite Line{26} = %i Using Progression
171     %.10g;\n', m+13,m+14,N(2),Prog);
172
172 L = 4*cuerda-(maxy+cuerda/4)*cos( alfa)-cuerda/2*sin( alfa);
173 Prog = mindist(Ymin*Prog5^(N(2)-1),L,N(4));
174   fprintf (fid , 'Line(27) = {%,%i}; Transfinite Line{27} = %i Using Progression
175     %.10g;\n', m+14,m+15,N(4),Prog);
175
176 %2D surfaces are defined from the previous lines.
177   fprintf (fid , 'Line Loop(3) = {3,10,16,-11};\n');
178   fprintf (fid , 'Ruled Surface(3) = {3};\n');
179   fprintf (fid , 'Transfinite Surface(3) = {%,%,%,%i};\n', m+1,m+2,m+4,m+5);
180
181   fprintf (fid , 'Line Loop(4) = {4,12,17,-13};\n');
182   fprintf (fid , 'Ruled Surface(4) = {4};\n');
183   fprintf (fid , 'Transfinite Surface(4) = {%,%,%,%i};\n', m+1,m+3,m+10,m+9);
184
185   fprintf (fid , 'Line Loop(5) = {-18,-11,8,20};\n');
186   fprintf (fid , 'Ruled Surface(5) = {5};\n');
187   fprintf (fid , 'Transfinite Surface(5) = {%,%,%,%i};\n', m+1,m+5,m+6,m+7);
188
189   fprintf (fid , 'Line Loop(6) = {-19,-13,8,21};\n');
190   fprintf (fid , 'Ruled Surface(6) = {6};\n');
191   fprintf (fid , 'Transfinite Surface(6) = {%,%,%,%i};\n', m+1,m+7,m+8,m+9);
192
193   fprintf (fid , 'Line Loop(7) = {5,14,-26,-9};\n');
194   fprintf (fid , 'Ruled Surface(7) = {7};\n');
195   fprintf (fid , 'Transfinite Surface(7) = {%,%,%,%i};\n', m+2,m+14,m+13,1);
196
197   fprintf (fid , 'Line Loop(8) = {6,15,-25,-9};\n');
198   fprintf (fid , 'Ruled Surface(8) = {8};\n');
199   fprintf (fid , 'Transfinite Surface(8) = {%,%,%,%i};\n', m+3,m+12,m+13,1);
200
201   fprintf (fid , 'Line Loop(9) = {14,27,-22,-10};\n');
202   fprintf (fid , 'Ruled Surface(9) = {9};\n');
203   fprintf (fid , 'Transfinite Surface(9) = {%,%,%,%i};\n', m+2,m+14,m+15,m+4);
204
205   fprintf (fid , 'Line Loop(10) = {15,24,-23,-12};\n');
206   fprintf (fid , 'Ruled Surface(10) = {10};\n');
207   fprintf (fid , 'Transfinite Surface(10) = {%,%,%,%i};\n', m+3,m+10,m+11,m+12);
208
209   fprintf (fid , 'Recombine Surface{1,2,3,4,5,6,7,8,9,10}=0;\n'); %This is important,
210     it tells Gmsh to attempt to join the default triangles into quadrangles
211     (2triangles=1quadrangle)
212
211 %The next lines extrude a small height the 2D surface to have a one-cell-depth
212   volume, necessary for finite volume codes. It is not necessary for finite
213   elements, but who uses them? :D
214   fprintf (fid , 'j1 [] = Extrude {0,0,%.10g} {Surface{1};Layers{1};Recombine;};\n',
215     cuerda/10);
213   fprintf (fid , 'j2 [] = Extrude {0,0,%.10g} {Surface{2};Layers{1};Recombine;};\n',
214     cuerda/10);
214   fprintf (fid , 'j3 [] = Extrude {0,0,%.10g} {Surface{3};Layers{1};Recombine;};\n',
215     cuerda/10);
215   fprintf (fid , 'j4 [] = Extrude {0,0,%.10g} {Surface{4};Layers{1};Recombine;};\n',
216     cuerda/10);

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216 fprintf (fid , 'j5 [] = Extrude {0,0,%10g} {Surface{5};Layers{1};Recombine;};\n' ,
217     cuerda/10);
218 fprintf (fid , 'j6 [] = Extrude {0,0,%10g} {Surface{6};Layers{1};Recombine;};\n' ,
219     cuerda/10);
220 fprintf (fid , 'j7 [] = Extrude {0,0,%10g} {Surface{7};Layers{1};Recombine;};\n' ,
221     cuerda/10);
222 fprintf (fid , 'j8 [] = Extrude {0,0,%10g} {Surface{8};Layers{1};Recombine;};\n' ,
223     cuerda/10);
224 fprintf (fid , 'j9 [] = Extrude {0,0,%10g} {Surface{9};Layers{1};Recombine;};\n' ,
225     cuerda/10);
226 fprintf (fid , 'j10 [] = Extrude {0,0,%10g} {Surface{10};Layers{1};Recombine;};\n' ,
227     cuerda/10);

228 %Grouping the faces and the volumes...
229 fprintf (fid , 'Physical Surface("inlet") = {j5[5],j6[5]};\n');
230 fprintf (fid , 'Physical Surface("outlet") = {j7[4],j8[4],j9[3],j10[3]};\n');
231 fprintf (fid , 'Physical Surface("airfoil") = {j1[2],j2[2]};\n');
232 fprintf (fid , 'Physical Surface("walls") =
233     {j3[4],j4[4],j5[2],j6[2],j9[4],j10[4]};\n');
234 fprintf (fid , 'Physical Surface("symmetry") =
235     {1,2,3,4,5,6,7,8,9,10,j1[0],j2[0],j3[0],j4[0],j5[0],j6[0],j7[0],j8[0],j9[0],j10[0]};\n');

236 printf (fid , 'Physical Volume("Volumen") =
237     {j1[1],j2[1],j3[1],j4[1],j5[1],j6[1],j7[1],j8[1],j9[1],j10[1]};\n');

238 fclose (fid);

239 N = N-1;
240 %In case you wonder, the info is just below:
241 printf ('The mesh is made of %i linear hexahedra.\n',
242         2*(N(1)*(N(2)+N(4))+N(4)*2*N(3)+N(2)*N(3)));
243 printf ('\n-----\n');
244 end

245
246
247 function Prog = mindist(Ymin,L,N)
248
249 %For a line of length L to be discretized in N elements, of which the shortest is
250 %at the beginning and has a length Ymin, we compute the Prog such that
251 %L=Ymin*sum(Prog^n, from n=0 to n=N). Ymin can be but is not limited to the
252 %Ymin defined in the next function.
253
254 e = 1;
255 Prog = 1.001;
256 while e > 0.001
257     Prog_t = Prog +
258         ((Prog^4-2*Prog^3+Prog^2)*L+(Prog^3-Prog^2+Prog^N*(Prog-Prog^2))*Ymin)/((Prog-1)*Prog^N*Ymin*N);
259     e = abs((Prog_t-Prog)/Prog);

```

```

258     Prog = Prog_t;
259
260     end
261
262     if  Prog < 1
263
264     Prog = 1;
265
266     end
267
268     end
269
270
271
272 %%%%%%%%%%%%%%
273
274
275
276     function Ymin = ypar (yplus ,cuerda ,Re,M,T0, eter)
277
278 %This function computes the minimum cell distance from a wall , according to
279 % equations for turbulent flow over a flat plate at zero incidence . It also
280 % computes some bonus data to define simulation parameters.
281
282     switch eter
283
284         case 'a'
285             T = T0/(1+0.2*M^2);
286             V = M*sqrt (1.4*287.074*T);
287             muT = 1.458e-6*T^1.5/(110.4+T);
288             rho = Re*muT/(V*cuerda);
289             P = rho*287.074*T;
290             P0 = P*(T0/T)^(1.4/0.4);
291             printf (' \n-----\n')
292             printf ('Medium: air\nRe = %g\nChord = %f [m]\nDensity = %g [Kg/m^3]\nDynamic
293             viscosity = %g [Kg/(ms)]\nFreestream speed = %f [m/s]\nFreestream Mach =
294             %f\nStatic pressure (absolute) = %f [Pa]\nStagnation pressure = %f
295             [Pa]\nTemperature = %f [K]\nStagnation temeprature = %f[K]\nY+ = %f\n\n',
296             Re,cuerda,rho ,muT,V,M,P,P0,T,T0,yplus)
297
298         case 'n'
299             T = T0/(1+0.2*M^2);
300             V = M*sqrt (1.4*297*T);
301             muT = 1.781e-5*(111+300.55)/(111+T)*(T/300.55)^1.5;
302             rho = Re*muT/(V*cuerda);
303             P = rho*297*T;
304             P0 = P*(T0/T)^(1.4/0.4);
305             printf (' \n-----\n')
306             printf ('Medium: nitrogen\nRe = %g\nChord = %f [m]\nDensity = %g
307             [Kg/m^3]\nDynamic viscosity = %g [Kg/(ms)]\nFreestream speed = %f
308             [m/s]\nFreestream Mach = %f\nStatic pressure (absolute) = %f
309             [Pa]\nStagnation pressure = %f [Pa]\nTemperature = %f [K]\nStagnation
310             temperature = %f [K]\nY+ = %f\n\n',
311             Re,cuerda,rho ,muT,V,M,P,P0,T,T0,yplus)
312
313         case 'h'

```



A. Additional codes

```
303 V = M;
304 rho = 1000*(1-(T0+288.9414)/(508929.2*(T0+68.12963))*(T0-3.9863)^2);
305 muT = rho*V*cuerda/Re;
306 printf ('\\n-----\\n');
307 printf ('Medium: water\\nRe = %g\\nChord = %f [m]\\nDensity = %g
308 [Kg/m^3]\\nDynamic viscosity = %g [Kg/(ms)]\\nFreestream speed = %f
309 [m/s]\\nTemperature = %f [K]\\nY+ = %f\\n\\n', Re,cuerda,rho,muT,V,yplus)
310 end
311 Cf = 0.02;
312
313 while i<10
314
315     funcion = 4.15*sqrt(Cf)*log10(Re*Cf)+1.7*sqrt(Cf)-1.0;
316     derfunc = (4.15*log10(exp(1.0))+0.5*4.15*log10(Re*Cf)+1.7/2.0)/sqrt(Cf);
317     fsd = funcion/derfunc;
318
319     if abs(fsd/Cf) <= exp(-5.0)
320         break
321     end
322
323     Cfo = Cf-fsd;
324
325     if Cfo <= 0.0
326         Cf = 0.5*Cf;
327     else
328         Cf = Cfo;
329     end
330
331     i=i+1;
332
333 end
334
335 %Cfo = (1./(4.15*log10(Re*Cf)+1.7))^2;
336 %tau = 0.5*rho*V*V*Cf
337 %aus = sqrt(tau/rho)
338
339 Ymin = yplus*muT/(V*sqrt(Cf/2));
340
341 printf ('To obtain CFL(max) <= 20 across the whole flowfield , a timestep dt <=
342 %10gs is recomended for transient simulations.\\n\\n', 20*Ymin/V)
343 printf ('The following values are recomended to initialize external flowfield
344 variables:\\nK = %g [m^2/s^2]\\nEpsilon = %g [m^2/s^3]\\nOmega = %g
345 [1/s]\\nTurbulent intensity = 6.6667e-7 [%]\\nHydraulic diameter = %f [m]\\n\\n',
346 1e-6*V^2,4.5e-7*V^3/cuerda,0.45*V/cuerda,0.0052164*cuerda)
347
348 end
```

Bibliography

- [1] *OpenFOAM, the open source CFD toolbox User Guide.* OpenFOAM, 2013.
- [2] B Mutlu Sumer and Jorgen Fredsoe. *Hydrodynamics around cylindrical structures.* World Scientific, 2006.